

Mechanics of randomly packed filaments—The “bird nest” as meta-material

Cite as: J. Appl. Phys. 127, 050902 (2020); doi: 10.1063/1.5132809

Submitted: 21 October 2019 · Accepted: 14 January 2020 ·

Published Online: 3 February 2020



N. Weiner,¹ Y. Bhosale,² M. Gazzola,^{2,3,a)} and H. King^{1,4,5,a)} 

AFFILIATIONS

¹Department of Polymer Science, University of Akron, Akron, Ohio 44325, USA

²Department of Mechanical Science and Engineering, University of Illinois at Urbana-Champaign, Urbana, Illinois 61801, USA

³National Center for Supercomputing Applications, University of Illinois at Urbana-Champaign, Urbana, Illinois 61801, USA

⁴Department of Biology, University of Akron, Akron, Ohio 44325, USA

⁵Biomimicry Research and Innovation Center, University of Akron, Akron, Ohio 44325, USA

^{a)}Authors to whom correspondence should be addressed: mgazzola@illinois.edu and hking@uakron.edu

ABSTRACT

Systems of randomly packed, macroscopic elements, from jammed spherical grains to tangled long filaments, represent a broad class of disordered meta-materials with a wide range of applications and manifestations in nature. A “bird nest” presents itself at an interface between hard round grains described by granular physics to long soft filaments, the center of textile material science. All of these randomly packed systems exhibit forms of self-assembly, evident through their robust packing statistics, and share a common elastoplastic response to oedometric compression. In reviewing packing statistics, mechanical response characterization, and consideration of boundary effects, we present a perspective that attempts to establish a link between the bulk and local behavior of a pile of sand and a wad of cotton, demonstrating the nest’s relationship with each. Finally, potential directions for impactful applications are outlined.

Published under license by AIP Publishing. <https://doi.org/10.1063/1.5132809>

I. INTRODUCTION

A. Observation of a nest

A cardinal uses its own body as a template in building its cup-nest. Found, filamentous materials are added and randomly packed against the bird-defined boundaries (see Fig. 1). The resulting structure is not strong, and one instinctively handles it delicately. Yet we know this structure has been given the profound responsibility of protecting the bird’s offspring. If defined as a random packing of elastic filaments, the bird nest is an unusual material: it is cohesive without attractive interactions; it is plastic although its elements are elastic; it is soft even if its filaments are hard. It embodies an instinctive understanding of granular mechanics, and yet it combines long flexible elements, impermanent frictional contacts, and boundary effects in a way that notably sets it apart from classical grain systems, as well as semiflexible polymer networks and other nonwoven materials, which derive mechanical response from permanent cross-links. How did this solution arise, what can we learn from it, and can it be usefully applied in an engineering context?

B. The nest as a construction template for novel materials

The history of changing environmental pressures has driven birds to their diversity of present day nesting solutions. A cooling climate led most to incubate with their own body heat; predation led many to do so in hidden locations up in the trees; and competition for convenient sites led to fabrication with lightweight (transportable by flight) materials.² Among the tree-nesting birds, some have spent millions of years working with fibers to build structures for protection and microclimatic regulation.^{3,4} Several needs drive bird nest design across the diversity of nests, but structural integrity under mechanical loads and disturbances, over its lifetime, is clearly a dominant factor. Large platform nests of eagles and hawks appear to derive stability from gravitational load of heavy sticks. Hummingbirds are known to use spiderweb as sticky lashing, and weavers learn to tie formal knots. Many birds, though, seem to rely on a fundamentally different strategy, rooted in the emergence of desirable properties of the disordered granular packing. The additional stick, selected based on some mechanical criteria, does not



FIG. 1. A cardinal nest easily supports the weight of the bird, as well as other perturbations: a cohesive granular structure made up of flimsy elastic filaments. Copyright 2016 Betty Wills (Atsme), licensed under a Wikimedia Commons CC-BY-SA 4.0 License.¹

serve to balance a torque or support an anticipated load, but rather contributes to the target material behavior of the aggregate. In doing so, they unknowingly apply nuances of scientific principles (learned instinctively through evolution²) that humans are only beginning to understand, and without need for abstraction, mechanically synthesize multifunctional meta-materials to suit their needs. Humans also build houses of wood, but their functionality derives from the coherent interaction of conceptually distinct parts (wall, supporting beam, envelope) as a structure. The cup nest represents a subtle shape with functionality mostly built into the material responses. Our *intelligent*, prescriptive design process has proven successful, but could only stand to benefit by emulating strategies of *naturally-selected* design, which rely on emergent properties of disordered matter.

The most basic concept underlying nest stability, by which randomly packed grains come to behave collectively as a solid, has only a couple decades ago been given a scientific name: “jamming.”⁵ This notion of a phase transition from fluid to disordered solid, in a system of athermal macroscopic elements, raises enough profound and fascinating questions to support a subfield of physics and an active line of research. The onset of jamming has been studied across diverse systems: foams, colloidal suspensions,⁶ and macroscopic elastic spheres.^{7,8} Some have considered the conceptual limit of “granular polymers”: floppy chains of hard beads with negligible bending stiffness, and large interparticle friction.^{9–14} A fundamental train of thought connects granular jamming to the glass transition¹⁵ and seeks to modify statistical mechanics to accommodate athermal analogs to characterize and predict the transition. Recent efforts have also been made to find generalities in jamming as it happens, i.e., to understand how jamming occurs, so as to usefully control its appearance and disappearance by design.¹⁶ We will not look at that closely here. *Instead, we will focus on statistically robust jammed*

states as tunable, versatile metamaterials. Indeed, the evolutionary value of the bird nest appears to be in the mechanical properties of its jammed state, specifically those emerging from a subtle interplay between geometry, elasticity, and friction between its slender, flexible elements. This presents opportunities for the development of light weight, compliant, shock absorbing materials made of recyclable components. If bird nest design is to be taken as inspiration for synthesis of a granular metamaterial with tunable mechanical properties, the role of flexibility, friction, and boundary effects at high aspect ratio should be carefully considered. As can be seen in Fig. 2, materials at the intersection of these features remain less explored, prompting us to ask the following questions:

- How do slender grains randomly pack? What does the robust, emergent state look like and what statistical parameters define it?
- How does that state mechanically behave? What is common among static and dynamic responses of granular packings, and how do they depend on grain properties? What is the role of flexibility in slender grains?
- How do boundary effects and packing protocols, critical when constitutive elements have sizes comparable to the whole system, modulate mechanical performance? Can we take advantage of boundaries, rather than seeing them as disturbances to bulk mechanics?

Answers could lead to minimal models and rational design guidelines to create lightweight materials with prescriptive, novel mechanical properties. Here, we aim to capture closest points of contact between these questions and the relevant scientific literature and emphasize gaps where useful insight should be found.

II. NESTS AS META-MATERIAL BETWEEN GRANULAR PACKINGS AND TEXTILES

A. Statistics of jammed state

Athermal grains lacking attractive interaction are capable of flowing around each other in response to external stress. If confined, however, they will readily “jam,” i.e., assume properties of a continuous solid, mechanically identified by the onset of rigidity. The jamming transition has been exploited for novel, practical applications in recent years, as reviewed in Ref. 16. The ability to change a material from solid to fluid by mechanical, rather than thermal, actuation has been implemented in the grasping mechanism of a granular based robotic gripper¹⁷ and in the propulsion of a soft robot.¹⁸ In response to sudden compressive strain, granular systems have been reported to propagate dynamic jamming fronts which, by straddling the transition, dissipate significant energy, thus demonstrating their value as shock absorbers.^{19,20} Potential value in the mechanics of the jammed state itself, and its tunability by variation of basic constituent characteristics has received less attention. Particularly, where that value and tunability derive from particle slenderness is the focus of our discussion.

In order to systematically characterize the structure and robustness of the jammed state, across the variety of grains, rods, and fibers considered, two statistical parameters are employed: (1) the volume fraction ϕ , defined as the ratio between the grains’ volume and total volume, measures how densely elements are packed; (2) the coordination number $\langle z \rangle$, defined as the average number of

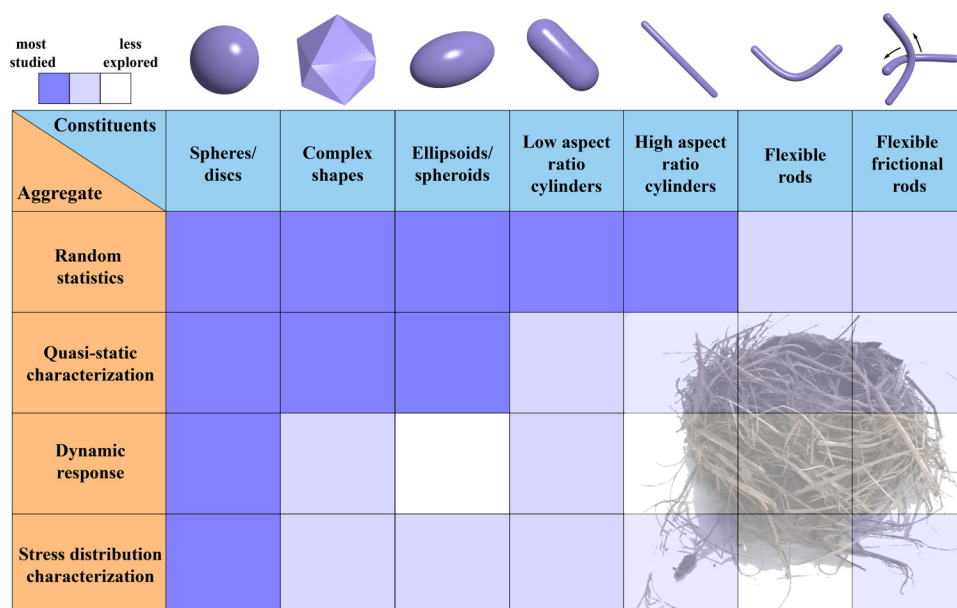


FIG. 2. Crude depiction of the relative degree that aggregate mechanical behaviors of packed, athermal particles have been studied for different types of constituent elements. The shading corresponds to the number of publications. “Bird nest”-like systems occupy the **less explored** region with flexible, frictional, high aspect ratio elements.

contacts per element, measures mechanical connectivity of the aggregate. Values of these parameters depend on the system’s confinement, preparation, and particle properties. Nonetheless, consistent trends across varying preparations are observed,²¹ demonstrating the role of self-assembly in the disordered packing, without which the characterization of generic jammed states would be tenuous. We now look at these trends across preparations of (1) hard, spherical, and spheroidal particles, (2) high aspect ratio, stiff rods, and (3) extremely slender and/or soft fibers typically associated with textiles, to identify similarities and departures, and contextualize the nature of “bird nest” materials.

Spheres have naturally received the most attention of the three cases. For the most dense regular (crystalline) packing, ϕ and $\langle z \rangle$ take values of exactly 0.74 and 12, respectively.²¹ Lack of orientational order, perhaps surprisingly, does not imply an arbitrary range of ϕ and $\langle z \rangle$. In fact, two distinct limits can be identified: random loose packed (RLP, $\phi \sim 0.55$)²² represents the limit of minimal mechanical stability under gravity; and random close packed (RCP, $\phi = 0.64$)²¹ is the densest state for which spheres can pack without crystallizing. Where an aggregate of spheres finds itself between these limits depends on friction and on how gently/vigorously it is packed but not sensitively on the details of the protocol.²³

Particle shape can play a role in both the geometry of the packed state and in the kinetics of the packing process. Slightly breaking spherical symmetry causes confined particles to rearrange by exerting torques on each other. Indeed, slightly oblate and prolate spheroids have been found to significantly deviate from spheres in packing fraction and coordination number. Results from simulations [Fig. 3(a)] show that as aspect ratio varies in either direction from unity, packing fraction first increases, reaching a maximum ($\phi \sim 0.72$) for moderately deformed grains, before trending downward.²⁴ The coordination number [Fig. 3(b)] is similarly minimal for

a sphere (for which $\langle z \rangle \sim 6$), but increases to a steady value of about 10 in either direction of aspect ratio. The results show that for increasingly prolate particles, packings become less dense, while the average number of contacts per particle necessary to prevent further compaction remains constant.

Intuitively, this behavior should, to some degree, extend to stiff cylinders of increasing aspect ratio. Experimental results for tinned buss wire, as shown in Figs. 3(c) and 3(d),²⁵ are qualitatively consistent. After some discrepancy at aspect ratios ≤ 10 , where edge effects are important, the number of contacts sufficient to maintain the jammed state saturates to $\langle z \rangle \sim 10$. The results agree with the geometry-based prediction of Ref. 26, in which ϕ is dependent only on the aspect ratio. They have also been supported by numerical simulations,²⁹ and appear to be generic (i.e., not strongly dependent on boundaries and packing protocol) as long as grain bending is negligible and pathological self-alignment is prevented.³⁰

At some ticklish point in increasing aspect ratio and/or flexibility, one intuitively wants to call the system “fibrous” rather than “granular.” While the transition point is far from clear, it would represent a bridge between two very different conceptual frameworks and language. Viewed from the perspective of network mechanics, a fibrous system could be considered a disordered and “entangled” subset.³¹ In that context, “entangled” distinguishes their impermanent, frictional contacts from permanent chemical bonds. “Entangled” can also alternatively refer to the continuous overlapping of extended particles’ rotational volumes,³² or the interpenetration of nonconvex particles,³³ which in either case inhibits their ability to rotate and rearrange with external stress.

Raw textile materials, whose constituent elements have aspect ratios three or four orders of magnitude larger³⁴ than the sticks of Figs. 3(c) and 3(d), clearly belong to the fibrous limit. Reducing to this smaller, slenderer scale has two effects: bending

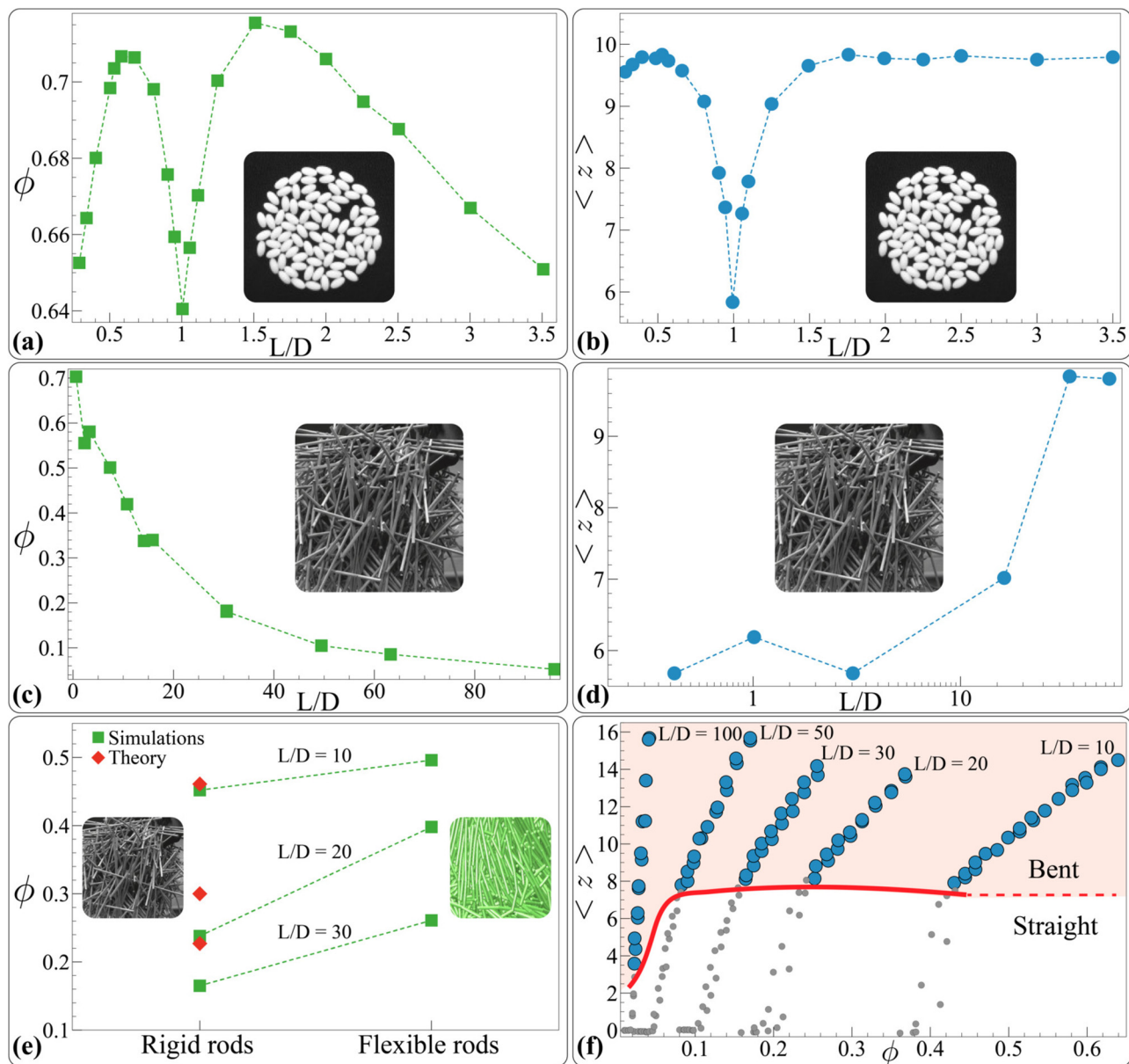


FIG. 3. Donev *et al.*²⁴ explored the effect of varying the aspect ratio, using oblate and prolate spheroids [(a) and (b)] on packing fraction ϕ and coordination number $\langle z \rangle$. Reproduced with permission from Donev *et al.*, *Science* **303**, 990–993 (2004). Copyright 2004 The American Association for the Advancement of Science. The case of high aspect ratio stiff rods has also been well explored both numerically and experimentally^{25,26} [(c) and (d)]. Reproduced with permission from J. Blouwolff and S. Fraden, *Europhys. Lett.* **76**, 1095 (2006). Copyright 2006 IOP Publishing. (e) DEM simulations demonstrate an increase in packing fraction for flexible rods when compared to rigid rods.²⁷ Reproduced with permission from Langston *et al.*, *Comput. Mater. Sci.* **96**, 108–116 (2015), licensed under a Creative Commons Attribution (CC BY) License. (f) Coordination number increases beyond the rigid rod limit for flexible rods pointing toward an entanglement transition, as observed in DEM simulations.²⁸ Reproduced with permission from Rodney *et al.*, *Phys. Rev. Lett.* **95**, 108004 (2005). Copyright 2005 American Physical Society.

rigidity drops to the point where packing itself introduces bending,^{35,36} unlike experiments with rigid rods; and friction becomes increasingly important compared to gravity/inertia, making it difficult to reach RCP by successive vertical excitations.

The latter issue makes comparison of asymptotic packing statistics ambiguous, so that pure granular and textile literature are somewhat disconnected. Nonetheless, a few studies, mostly computational, underscore potential bridges.

An increase in packing fraction can be seen in Fig. 3(e), for Discrete Element Method (DEM) simulations of rods with increasing flexibility, loaded under gravity.²⁷ The sticks constrained from bending show values in agreement with theory^{26,37} for stiff rods. Introducing flexibility, unsurprisingly, allows rods to pack to volume fractions beyond those seen for rigid rods, as rods are able to locally reorient during packing.

Figure 3(f) reports numerical simulation results of contact number and volume fraction for flexible rods of varying aspect ratios under isostatic compression.²⁸ Below the red line, rods pack and rearrange without activating bending modes. Pushed beyond a critical volume fraction, however, finite bending energy is measured in the fibers, indicating onset of what they call “entanglement.” Notably, the packing fraction at the transition is quantitatively consistent with rigid rod RCP values in Fig. 3(c), but the contact numbers disagree with those of Fig. 3(d), both quantitatively and in the trend with increasing aspect ratio. Upon further compression beyond the transition, an additionally important role of flexibility is seen, as the contact number starts growing linearly with the packing fraction, beyond the rigid rod limit.

Granular physics extends the conceptual framework of statistical mechanics to athermal systems by describing many particle

ensembles as materials. In simply looking at how they pack under generic confinement, we see that sticks and fibers can be described by the same average parameters used to describe jammed spheres. In that space, a nestlike material occupies a region of predictably low density and asymptotically high contact number. The process that brings them there is dependent mostly on particle geometry; flexibility introduces another degree of freedom in further deformation of the aggregate.

B. Mechanical response

Section II A served to identify macrostates of the systems for which we anticipate reproducible behavior. We now explore simple mechanical characterization of those states, for packings of plastic “spheroids” of aspect ratio $\lesssim 2$, wooden “rods” of aspect ratio ~ 50 , and natural raw cotton “fibers” with high aspect ratio ~ 1000 .

A recent study by Parafiniuk *et al.* looked at the stress response of packed spheroids to successive, cyclic, oedometric compression.³⁸ The results, shown in Fig. 4(a), reveal some noteworthy qualitative features. The first cycle (bold black) loads and unloads nonlinearly, carving out a large hysteretic loop and returns to a shifted zero-stress state. Nonlinearity is expected as deformation

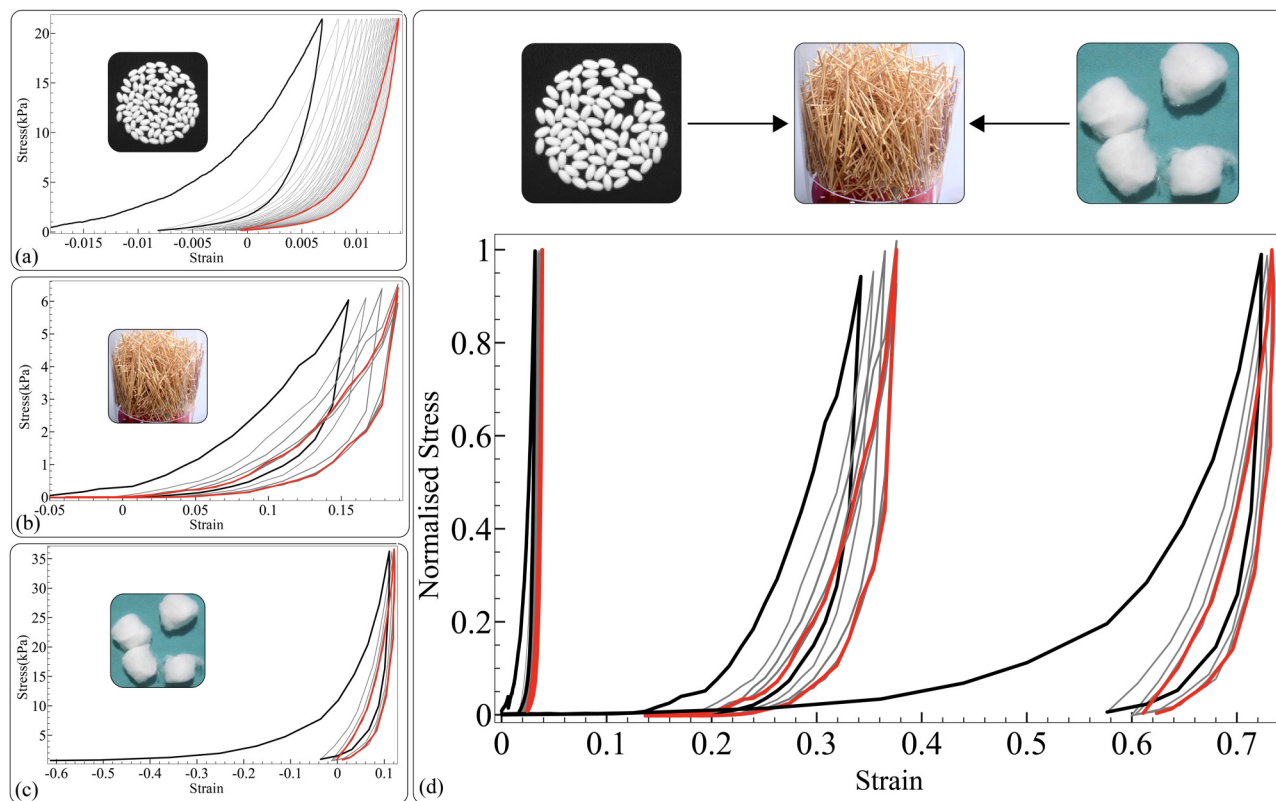


FIG. 4. The same qualitative behavior can be seen in the stress strain data for (a) low aspect ratio spheroids.³⁸ Reproduced with permission from Parafiniuk *et al.*, *Physica A* **501**, 1–11 (2018). Copyright 2018 Elsevier. (b) High aspect ratio rods (c) and raw cotton fibers.³⁴ Reproduced with permission from Poquillon *et al.*, *J. Mater. Sci.* **40**, 5963–5970 (2005). Copyright 2005 Springer Nature. (d) When plotted on the same normalized stress scales, the difference in plastic strain becomes evident.

can increase the number of contacts between grains (increasing force chain density), and because the contact forces themselves are Hertzian.³⁹ The subsequent cycles (gray) feature progressively decreasing plasticity, as the aggregate gradually compacts. In this context, *plasticity is a meta-material property*, in that it does not involve damage of primary material. Instead, it results from rearrangement, attributed to decreasing orientational disorder,³⁸ as the system moves from an initially somewhat loose packing (near RLP) formed during its preparation toward its random close packed (RCP) limit. Here, between first and final cycle, the packing fraction increases from ~ 0.54 to ~ 0.56 .

When plastic deformation stops, finite hysteresis remains. This persistent energy loss has been attributed to *reversible* microslippage of frictional contacts.⁴⁰ The mechanism would be quasistatic, involving static friction. As the aggregate loads and deforms, a given interparticle contact experiences shear. Upon overcoming static friction, the contact slides to a new equilibrium position. The contact returns to its original positions as the load is relieved but only after overcoming static friction in the opposite direction. The return trip is less “springy” because the previous deformation is still temporarily stored in the network of frictional contacts.

For higher aspect ratio rods, flexibility plays a quantitative role in the mechanical response without changing the qualitative behavior from that of spheroids. Unpublished data for bamboo rods with aspect ratio 50 [Fig. 4(b)] shows initial plasticity in the first few cycles eventually giving way to a steady state cycle with hysteresis. The observed plasticity indicates that the initial state of the system was slightly looser ($\phi = 0.071$) than the asymptotic value, and compacted under compression closer to that limit ($\phi = 0.079$), which is consistent with values from Ref. 25 ($\phi = 0.1$), but again lower due to confinement effects. Figure 4(d) shows the data for spheroids³⁸ and for our rods together, emphasizing the different scales of plasticity between the two systems. Though the magnitude of applied stress differs significantly, the extent of final compaction appears not to depend on it: the respective asymptotic packing limits are approximately reached in either case.

Response of conventional fibers, with a much higher aspect ratio ~ 1000 , to oedometric compression has been reported by Ref. 34. As shown in Fig. 4(c), these display the same qualitative behaviors as those of both spheroid assemblies and slender rods: initial plasticity followed by a steady state cycle with hysteresis, a behavior first reported for textile materials by Van Wyk in the 1940s.⁴¹ Again, increasing to more slender, more flexible fibers (i.e., lower effective bending stiffness) shifts the results quantitatively. For small, fine fibers, gravitational and inertial forces are less sufficient to overcome frictional contacts, which leads to a much looser initial state, and therefore larger room for plasticity in compression.

Another investigation of fiber wads in uniaxial compression provides a micromechanical picture of the trend in Fig. 4(c), in two distinct steps. First, fibers in an initially loose, random, 3D network bend and reorient away from the axis of compression, softly resisting with large plasticity. By the end of the cycle, the system behaves as a 2D mat, largely aligned perpendicular to compression, displaying greater stiffness and low plasticity.⁴²

Where friction at loaded, impermanent contacts appears to be the common feature of granular/fibrous systems, which leads to their shared, distinctive plastic and hysteretic responses to successive

quasistatic compression, slenderness appears to play a quantitative role. Increasing grain slenderness not only introduces a new (bending) mode of particle deformation, through which stresses are translated from contact to contact, it also introduces different time scales to the system. Both should have consequences on the dynamic response of the aggregate.

For jammed grains to exhibit stiffness, stress must be propagated from grain to grain. For spheres, stress is communicated through compressive deformations of successive grains in loaded contact. This allows for an impulse to travel along a chain of contacts at speeds proportional to the square root of the stiffness of the Hertzian contacts.⁴³ For rods, a loaded contact exerts a torque on the portion of rod between itself and the nearest contacts which hold it in place. A pulse, then, necessarily travels through many perpendicular paths mediated by the bending stiffness of the rod. For very high aspect ratio, the distance between contacts becomes large relative to rod diameter h , and the bending stiffness decreases with h^4 . The combined factors must both lower the speed of propagation and increase the transverse diffusion of sudden stress. The dissipation mechanism we described in the context of quasistatic compression is not inherently dependent on strain rate (as would be the case for a viscoelastic material) but rather originates from the sequence of local deformations which lock and release frictional contacts. This implies that both storage and dissipation of energy from dynamic forcing would be nontrivially dependent on the frequency. At the same time, by manipulating the stiffness and geometry of slender rods, length and time scales could be injected in a controlled way, providing tunability of the dynamic response.

C. Internal stresses and boundary effects

In the case of high aspect ratio elastic rods in a realistic nest, the notion of bulk properties becomes less clear and the role of boundaries becomes more central. In this context, how does the nest relate to grains and fibers? For mostly round grains, the relationship between internal stresses and external boundaries was characterized in 1895, with Janssen’s investigation of the fractional weight of grains supported by the walls of a silo [Fig. 5(a)].⁴⁷ Though the grains flow like a fluid as they are added to the container, the pressure at the bottom, rather than increasing linearly with the filling height of grains, saturates in the form of an exponential $1 - e^{-\lambda z}$. The relationship between the vertical pressure σ_{zz} and height z from the top revealed a generic behavior dependent only on the parameter λ or the decay length which depends on the pressure ratio κ , which arises from particle shape, wall geometry, and friction.

The more recently developed force chain motif⁴⁸ complements this observation to complete an intuitive story. As grains are added, contacts are formed until they meet the isostatic stability condition. Increasing load on the disordered contacts focuses stress into heterogeneous 1D load structures between grains, which propagate through the material and end on the silo walls. The end of the force chain exerts a normal force on the vertical wall, and through static friction relieves some of the total weight on the bottom. Removal of the walls means breaking the force chains from their ends, losing the stability condition, and flowing—in other words, unjamming.

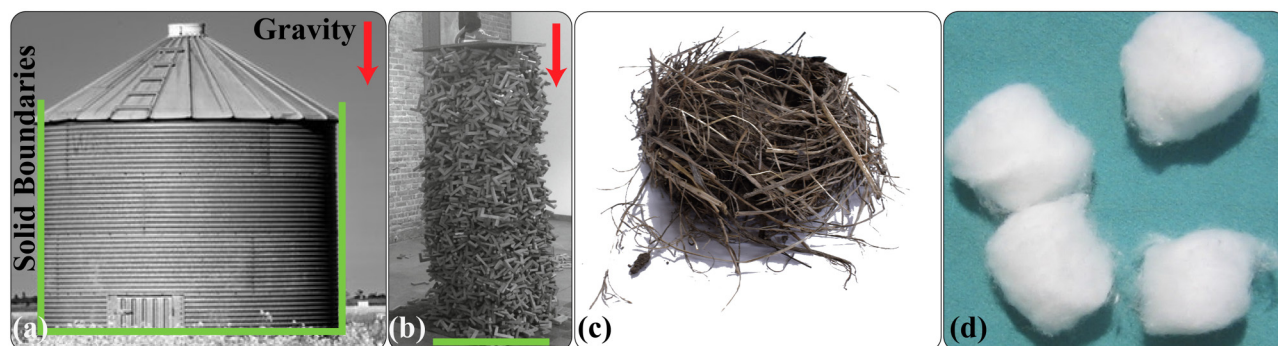


FIG. 5. (a) Grains jammed by multiple boundaries under gravity in a grain silo.⁴⁴ (b) A structure jammed solely by the bottom wall and gravity made up of Z-form shapes.⁴⁵ Reproduced with permission from Murphy *et al.* *Archit. Des.* **87**, 74–81 (2017). Copyright 2017 John Wiley and Sons. (c) A bird's nest stable without any external forcing or boundaries. Poquillon *et al.*, *J. Mater. Res.* **40**, 5963–5970 (2005). Copyright 2005 Cambridge. (d) A piece of cotton fiber stable without any external forcing or boundaries. Copyright 2008 licensed under a Wikimedia Commons CC-BY-SA 3.0 License.⁴⁶

This picture fails at some point for anisotropic grain shapes. For extended particles with kinks, random packing causes interpenetration and entanglement, which complicate the stability condition by nontrivially coupling torques and normal contacts.^{33,49} For spheres, torques are mediated only by friction, but hooked particles must both rotate and translate in order to flow past each other. Columns of hooked grains can be stable without walls and can bear loads beyond their own weight, as shown in Fig. 5(b). These columns and arches are reminiscent of sturdy platform nests, with contacts ultimately loaded by gravity. The analogous stress-propagating motif for this more complicated case must still end at the lower external boundary to maintain force balance for gravity and for the existence of a stable nonaccelerating disordered interlocked structure.

Some cup nests, by contrast, can be turned upside-down, or even thrown against a wall without falling apart [Fig. 5(c)]. This implies a jammed state that persists without any external confinement. This situation is not easily compatible with the generic jamming mechanism described above, as there is no external force to load internal contacts nor a boundary for the analogous “force chain” to lean on. One plausible explanation involves the additional role of flexibility in the construction process. If sticks are forced to bend while packing, some of this bending stress could be stored in the system, held by frictional contacts. The resulting motif of stress propagation in the material would be highly complex, but it could, in principle, satisfy force balance with internal stresses, as a disordered version of a “stick bomb.”⁵⁰ Though there is no indication that self-stress is induced in the artificial samples analyzed in Secs. II A and II B, its likely presence in natural bird nests would place them in better company with unwoven textile materials such as felt⁵¹—disordered tangles of fiber whose mechanics derive from contacts loaded by internal bending stresses [Fig. 5(d)]. When and how the force chain motif of the granular case, which requires boundaries for stability, is replaced by its analog for entangled fibers, in which a free floating sturdy structure is stabilized by bending modes remains an intriguing question for future research.

III. MATERIAL DESIGN AND ROLE OF SIMULATIONS

As illustrated in Secs. I and II, “bird nest” systems may provide a route towards light weight, tunable, and versatile metamaterials. The key to harness these opportunities lies in establishing a systematic and efficient way to design packing systems (and confinement strategies) to meet desired target behaviors. Given the lack of theory guiding us, our poor physical understanding of the mechanisms at play, and the overall system complexity, computational modeling may prove to be a powerful asset. Indeed, nest systems are characterized by a number of critical variables, from the geometric and material properties of their constituents to their boundary conditions. This vast space can hardly be explored experimentally. Hence the need for predictive and efficient numerical models to complement and systematically integrate necessary experiments. Finite element methods have been employed for the simulation of disordered systems characterized by cylindrical elements of varying aspect ratios. Although characterized by the highest level of fidelity, such methods are computationally expensive, rendering them impractical for the exploration of a vast design space. Alternative modeling approaches leverage the slender nature of fibers.⁵² These objects are then treated as one-dimensional systems, moving away from three-dimensional elasticity and significantly reducing the complexity of their mathematical representation. As a direct consequence, one-dimensional models are computationally inexpensive. Several approximations have been proposed, from simple spring-mass systems able to capture stretching and bending modes at first order, to discrete rod models⁵³ that accurately capture dynamics in three-dimensional space, accounting for various modes of deformation. The graphics community has been most active in this area, where the use of Cosserat model⁵² and its (far more popular) unstretchable and unshearable counterpart, the Kirchhoff model,⁵⁴ have led to realistic simulations of elastic ribbons,^{55,56} woven cloth^{57,58} [Fig. 6(d)], entangled hair and fibers^{56,59} [Fig. 6(a)], wire mesh,⁶⁰ etc. These models also found application in physics, biology and engineering to characterize polymers and DNA,^{61,62} flagella,⁶³

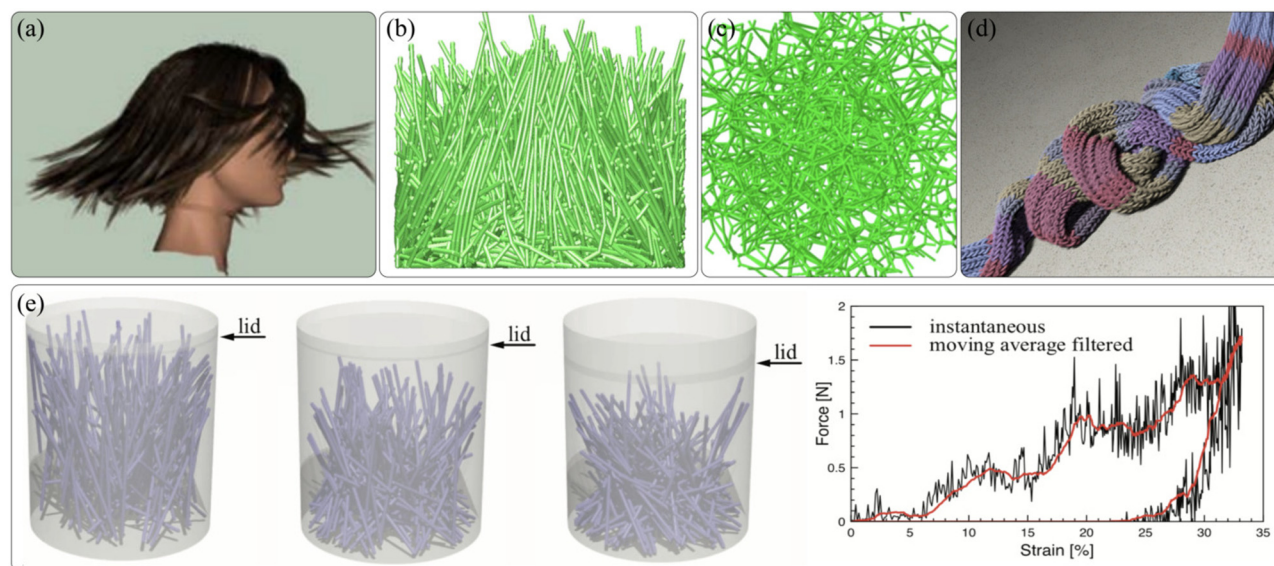


FIG. 6. Simulations of (a) natural hair.⁵⁶ Reproduced with permission from Bertails *et al.*, *ACM Trans. Graph.* **25**, 1180–1187 (2006). Copyright 2006 Association for Computing Machinery. (b) Packing of flexible fibers.²⁷ Reproduced with permission from Langston *et al.*, *Comput. Mater. Sci.* **96**, 108–116 (2015). Copyright 2015 Langston, licensed under a Creative Commons Attribution (CC BY) License. (c) Fungal mycelium.⁷³ Reproduced with permission from Islam *et al.*, *Sci. Rep.* **7**, 13070 (2017). Copyright 2017 Islam, licensed under a Creative Commons Attribution (CC BY) License. (d) Knitted cloth at yarn level.⁵⁸ Reproduced with permission from Kaldor *et al.*, *ACM Trans. Graph.* **27**, 65 (2008). Copyright 2008 Association for Computing Machinery. (e) A quasistatic compressive strain cycle for 250 rods and corresponding load–strain curve.

tendrils,⁶⁴ mycelium networks⁶⁵, cables in automotive design,⁶⁶ soft robot arms,⁶⁷ and dynamic musculoskeletal architectures.^{68–72}

These representations are versatile and accurate, can be easily interfaced with dynamic environmental loads (contact, friction, hydrodynamics), and significantly reduce complexity and computational costs, in particular, relative to standard approaches based on finite element methods. Figure 6(e) illustrates that this approach can be adopted to the study of nest systems. There, we considered thin, virtual wooden sticks characterized by circular cross sections and with bending stiffness comparable to the setup of Fig. 4(b). Friction among sticks was assumed to be isotropic and estimated through friction tests. Contacts were also detected and accounted for through a repulsive force. Finally, for simplicity, the sticks–container interaction was modeled as the stick–stick interaction. We then simulated a cycle of compression and recorded the “nest” response on the lid of the container. As can be noticed in Fig. 6(e), the generated load–strain curve qualitatively captures the highly hysteretic behavior of Fig. 4(b). We note that because of the limited number of rods employed (250), the load measurements are noisier than the experiments; nevertheless, the trend is clearly captured.

These techniques thus can be employed to “preview” in-silico (forward design) dynamic behavior of a given aggregate. At the same time, given their moderate computational costs and numerical robustness, they are also suitable to perform inverse design tasks, in which key properties of the aggregate are identified in order to achieve an overall target system’s behavior. In this context, the use of evolutionary strategies is particularly promising. These

class of algorithms generate populations of candidate solutions (i.e., different nest systems). These are simulated independently from each other (allowing us to distribute them across supercomputing facilities) and their dynamic response is evaluated according to a desired metric. The best solutions are then recombined, to generate a new, more performant pool of aggregates, until no significant improvement is observed. We have employed these procedures in combination to Cosserat models, to improve the locomotory performance of soft-robots,^{70–72} demonstrating the practical viability of this approach.

IV. OUTLOOK

This perspective paper aims at contextualizing nestlike aggregates as materials, characterized by rich dynamic behaviors at an unknown transition between classic hard grains and textile fibers. As such, they may provide an avenue to bridge the range of applications typically associated with these apparently disparate systems.

Much work has focused on the drivers, implications, and characteristics of the jamming transition in grains. Manipulation of the transition, back and forth between fluidlike and solidlike properties via external confinement has presented a basis of actuation in soft robotics^{17,80,81} and deformable aerostructures.⁸² Architects and artists have recently demonstrated the elegance and practical versatility that comes with embracing disorder and self-assembly instead of prescriptive control to build reconfigurable structures of emergent stability. This has been demonstrated both through choice of particle geometry^{45,75,83} and composite granular/fibrous building material.^{77,84} The

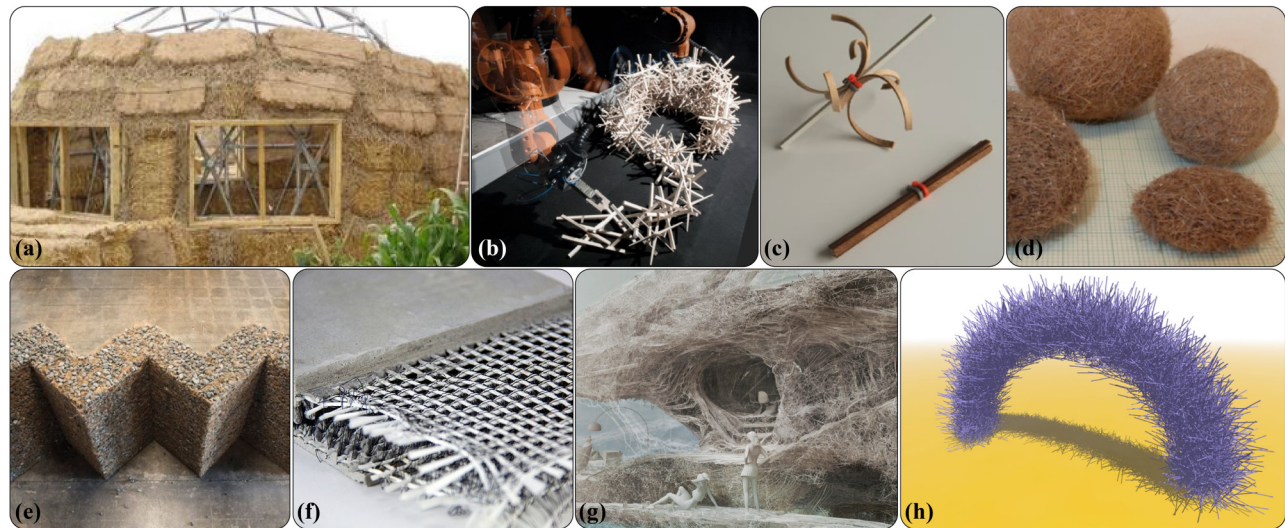


FIG. 7. (a) Straw-bale based construction,⁷⁴ (b) adaptive structure built using interlocking particles,⁷⁵ (c) particles changing shape based on a hygroscopic response.⁷⁵ Reproduced with permission from K. Dierichs and A. Menges, *Archit. Des.* **87**, 88–93 (2017). Copyright 2017 John Wiley and Sons. (d) Aegagropilae, an entangled fiber network formed from dead sea grass in the ocean.⁷⁶ Reproduced with permission from Verhille *et al.*, *Proc. Natl. Acad. Sci.* **114**, 4607–4612 (2017). Copyright 2017 National Academy of Sciences. (e) Stable granular structures built using rope as internal confinement.⁷⁷ Reproduced with permission from Aejmelaeus-Lindström *et al.*, *Archit. Des.* **87**, 82–87 (2017). Copyright 2017 John Wiley and Sons. (f) Image of fiber reinforced concrete.⁷⁸ Copyright 2013 R. Thyroff, licensed under a Wikimedia Commons CC-BY-SA 3.0 License. (g) Fiber based architectural design of a modern house.⁷⁹ Reproduced with permission from Retsin, *Archit. Des.* **86**, 84–89 (2016). Copyright 2016 John Wiley and Sons. (h) Adaptive, flexible, and tunable arch made of granular flexible rods.

term “Aleatory architectures” has been coined⁸⁵ to describe this new approach to engineering, in which the building materials are disordered and reconfigurable (by unjamming). Where these and other applications make use of when and how grains jam, the richness in their mechanical response to deformation has not been harnessed to similar effect. By controlling slenderness and flexibility in even simple shapes, this richness can be explored.

On the other hand, understanding mechanics of entangled random fiber networks has been at the core of development in textiles,^{34,86} ballistic impact mitigation,^{87,88} fiber based architecture⁸⁹ [Fig. 7(g)] and construction.⁹⁰ Use of compressed, randomly packed hay bales as building material [commonly termed as straw-bale construction, Fig. 7(a)]⁹¹ has been revived as an environment friendly option for construction, providing structure and insulation. Naturally occurring examples will continue to provide insight toward intelligent application. Under water, buoyancy and random flows can cause fibrous structures to passively self-assemble. Aegagropilae [Fig. 7(d)]—balls of dead, sea grass which are gradually entangled and packed by random ocean currents—appear mechanically very similar to continuous, cohesive, elastic spheres. The scaling of their effective modulus with mean density has been effectively modeled based on filament bending stiffness and contact number.⁷⁶

Real bird nests have inspired scientific study for hundreds of years, but the underlying logic from a practical, physical perspective is coming closer to focus with research into both nest structure and building behavior. While several forces have been shown to drive bird nest design^{3,92–94} across the diversity of nests,^{95,96}

the need for structural integrity under mechanical loads and disturbances, over the lifetime of the nest, is seen as a dominant factor.⁹⁷ Some of the intense complexity of weaver nest morphology has been found to emerge, in part, from processes involving simple construction rules and self-organizing mechanisms such as stigmergy.⁹⁸ Observations of the nesting behavior in zebra finches show selection criteria based on filament geometry and flexibility.^{99,100} Further cross-disciplinary study of bird nesting behavior, with controlled material inputs, output mechanical characterization, and complementary experiments and simulations of artificial analogs, could reveal generalizable construction algorithms of significant biological and technological impact.

Between sand and cloth, at a blurry interface between granular and textile mechanics, exists a class of material familiar to the biological world but relatively unexplored with scientific rigor. Understanding this region of parameter space could generate new points of theoretical traction into granular physics, illuminate functional mechanisms in animal engineering that extend beyond birds and biological curiosity, and inform design of lightweight metamaterials with prescriptive mechanical properties that cut through many areas of high current importance: civil engineering and architectures (reliable, inexpensive, reusable, and self-repairing construction materials), transportation (lightweight composites, shock absorbers), and advanced manufacturing.

AUTHORS' CONTRIBUTIONS

N. W. and Y. B. contributed equally to this manuscript.

ACKNOWLEDGMENTS

The authors acknowledge support by the Blue Waters project (OCI- 0725070, ACI-1238993), a joint effort of the University of Illinois at Urbana-Champaign and its National Center for Supercomputing Applications. This work used the Extreme Science and Engineering Discovery Environment (XSEDE) Stampede2, supported by National Science Foundation grant number ACI-1548562, at the Texas Advanced Computing Center (TACC) through allocation TG-MCB190004. This work was financially supported by the National Science Foundation (NSF) (Award No. ENG-1825440).

REFERENCES

- ¹B. Wills, see https://commons.wikimedia.org/wiki/File:Cardinal_babies.jpg for more information about “Cardinal babies.”
- ²N. E. Collias, “The evolution of nests and nest-building in birds,” *Am. Zool.* **4**, 175–190 (1964).
- ³M. C. Mainwaring, I. R. Hartley, M. M. Lambrechts, and D. C. Deeming, “The design and function of birds’ nests,” *Ecol. Evol.* **4**, 3909–3928 (2014).
- ⁴N. E. Collias, “On the origin and evolution of nest building by passerine birds,” *Condor* **99**, 253–270 (1997).
- ⁵R. Ball and J. Melrose, “Lubrication breakdown in hydrodynamic simulations of concentrated colloids,” *Adv. Colloid Interface Sci.* **59**, 19–30 (1995).
- ⁶V. Trappe, V. Prasad, L. Cipelletti, P. Segre, and D. A. Weitz, “Jamming phase diagram for attractive particles,” *Nature* **411**, 772 (2001).
- ⁷A. J. Liu and S. R. Nagel, “The jamming transition and the marginally jammed solid,” *Annu. Rev. Condens. Matter Phys.* **1**, 347–369 (2010).
- ⁸M. van Hecke, “Jamming of soft particles: Geometry, mechanics, scaling and isotaticity,” *J. Phys. Condens. Matter* **22**, 033101 (2009).
- ⁹C. J. O. Reichhardt and L. M. Lopatina, “A ball-and-chain polymer model,” *Science* **326**, 374–375 (2009).
- ¹⁰L. M. Lopatina, C. J. Olson Reichhardt, and C. Reichhardt, “Jamming in granular polymers,” *Phys. Rev. E* **84**, 011303 (2011).
- ¹¹L.-N. Zou, X. Cheng, M. L. Rivers, H. M. Jaeger, and S. R. Nagel, “The packing of granular polymer chains,” *Science* **326**, 408–410 (2009).
- ¹²E. Brown, A. Nasto, A. G. Athanassiadis, and H. M. Jaeger, “Strain stiffening in random packings of entangled granular chains,” *Phys. Rev. Lett.* **108**, 108302 (2012).
- ¹³D. Dumont, M. Houze, P. Rambach, T. Salez, S. Patinet, and P. Damman, “Emergent strain stiffening in interlocked granular chains,” *Phys. Rev. Lett.* **120**, 088001 (2018).
- ¹⁴A. Mohaddespour and R. J. Hill, “Granular polymer composites,” *Soft Matter* **8**, 12060–12065 (2012).
- ¹⁵A. J. Liu and S. R. Nagel, “Jamming is not just cool anymore,” *Nature* **396**, 21–22 (1998).
- ¹⁶H. M. Jaeger, “Celebrating soft matter’s 10th anniversary: Toward jamming by design,” *Soft Matter* **11**, 12–27 (2015).
- ¹⁷E. Brown, N. Rodenberg, J. Amend, A. Mozeika, E. Steltz, M. R. Zakin, H. Lipson, and H. M. Jaeger, “Universal robotic gripper based on the jamming of granular material,” *Proc. Natl. Acad. Sci. U.S.A.* **107**, 18809–18814 (2010).
- ¹⁸E. Steltz, A. Mozeika, J. Rembisz, N. Corson, and H. Jaeger, “Jamming as an enabling technology for soft robotics,” in *Electroactive Polymer Actuators and Devices (EAPAD) 2010* (International Society for Optics and Photonics, 2010), Vol. 7642, p. 764225.
- ¹⁹L. R. Gómez, A. M. Turner, and V. Vitelli, “Uniform shock waves in disordered granular matter,” *Phys. Rev. E* **86**, 041302 (2012).
- ²⁰L. R. Gómez, A. M. Turner, M. van Hecke, and V. Vitelli, “Shocks near jamming,” *Phys. Rev. Lett.* **108**, 058001 (2012).
- ²¹G. Scott and D. Kilgour, “The density of random close packing of spheres,” *J. Phys. D Appl. Phys.* **2**, 863 (1969).
- ²²G. Y. Onoda and E. G. Liniger, “Random loose packings of uniform spheres and the dilatancy onset,” *Phys. Rev. Lett.* **64**, 2727–2730 (1990).
- ²³G. R. Farrell, K. M. Martini, and N. Menon, “Loose packings of frictional spheres,” *Soft Matter* **6**, 2925–2930 (2010).
- ²⁴A. Donev, I. Cisse, D. Sachs, E. A. Varniano, F. H. Stillinger, R. Connelly, S. Torquato, and P. M. Chaikin, “Improving the density of jammed disordered packings using ellipsoids,” *Science* **303**, 990–993 (2004).
- ²⁵J. Blouwolf and S. Fraden, “The coordination number of granular cylinders,” *Europhys. Lett.* **76**, 1095 (2006).
- ²⁶A. P. Philipse, “The random contact equation and its implications for (colloidal) rods in packings, suspensions, and anisotropic powders,” *Langmuir* **12**, 1127–1133 (1996).
- ²⁷P. Langston, A. R. Kennedy, and H. Constantin, “Discrete element modelling of flexible fibre packing,” *Comput. Mater. Sci.* **96**, 108–116 (2015).
- ²⁸D. Rodney, M. Fivel, and R. Dendievel, “Discrete modeling of the mechanics of entangled materials,” *Phys. Rev. Lett.* **95**, 108004 (2005).
- ²⁹S. Williams and A. Philipse, “Random packings of spheres and spherocylinders simulated by mechanical contraction,” *Phys. Rev. E* **67**, 051301 (2003).
- ³⁰F. X. Villarruel, B. E. Lauderdale, D. M. Mueth, and H. M. Jaeger, “Compaction of rods: Relaxation and ordering in vibrated, anisotropic granular material,” *Phys. Rev. E* **61**, 6914 (2000).
- ³¹R. C. Picu, “Mechanics of random fiber networks—A review,” *Soft Matter* **7**, 6768–6785 (2011).
- ³²A. M. Wierenga and A. P. Philipse, “Low-shear viscosity of isotropic dispersions of (Brownian) rods and fibres: A review of theory and experiments,” *Colloids Surf. A* **137**, 355–372 (1998).
- ³³N. Gravish, S. V. Franklin, D. L. Hu, and D. I. Goldman, “Entangled granular media,” *Phys. Rev. Lett.* **108**, 208001 (2012).
- ³⁴D. Poquillon, B. Viguier, and E. Andrieu, “Experimental data about mechanical behaviour during compression tests for various matted fibres,” *J. Mater. Sci.* **40**, 5963–5970 (2005).
- ³⁵R. A. Asad, W. Yu, Y.-H. Zheng, and Y. He, “Characterization of prickly tactile discomfort properties of different textile single fibers using an axial fiber-compression-bending analyzer (FICBA),” *Text. Res. J.* **85**, 512–523 (2015).
- ³⁶J. W. Hearle and W. E. Morton, *Physical Properties of Textile Fibres* (Elsevier, 2008).
- ³⁷J. Parkhouse and A. Kelly, “The random packing of fibres in three dimensions,” *Proc. R. Soc. A* **451**, 737–746 (1995).
- ³⁸P. Parafiniuk, M. Bańda, M. Stasiak, J. Horabik, J. Wiacek, and M. Molenda, “Effect of aspect ratio on the mechanical behavior of packings of spheroids,” *Physica A* **501**, 1–11 (2018).
- ³⁹K. L. Johnson and K. L. Johnson, *Contact Mechanics* (Cambridge University Press, 1987).
- ⁴⁰M. H. Khalili, J.-N. Roux, J.-M. Pereira, S. Brisard, and M. Bornert, “Numerical study of one-dimensional compression of granular materials. I. Stress-strain behavior, microstructure, and irreversibility,” *Phys. Rev. E* **95**, 032907 (2017).
- ⁴¹C. Van Wyk, “20—Note on the compressibility of wool,” *J. Text. Inst. Trans.* **37**, T285–T292 (1946).
- ⁴²S. Toll, “Packing mechanics of fiber reinforcements,” *Polym. Eng. Sci.* **38**, 1337–1350 (1998).
- ⁴³E. T. Owens and K. E. Daniels, “Sound propagation and force chains in granular materials,” *Europhys. Lett.* **94**, 54005 (2011).
- ⁴⁴L. T. Deneen, see <https://www.pexels.com/photo/metal-building-grayscale-photo-1058397/> for more information about “Metal building grayscale photo.”
- ⁴⁵K. Murphy, L. Roth, D. Peterman, and H. Jaeger, “Aleatory construction based on jamming: Stability through self-confinement,” *Archit. Des.* **87**, 74–81 (2017).
- ⁴⁶See [https://commons.wikimedia.org/wiki/File:Three_bamboo_skews_six_cottonballs_one_screencleaning_chamois\(used_but_not_moist\).jpg](https://commons.wikimedia.org/wiki/File:Three_bamboo_skews_six_cottonballs_one_screencleaning_chamois(used_but_not_moist).jpg) for more information about “Three bamboo skewers six cottonballs one screencleaning chamois (used but not moist).”
- ⁴⁷M. Sperl, “Experiments on corn pressure in silo cells—Translation and comment of Janssen’s paper from 1895,” *Gran. Matter* **8**, 59–65 (2006).
- ⁴⁸T. S. Majmudar and R. P. Behringer, “Contact force measurements and stress-induced anisotropy in granular materials,” *Nature* **435**, 1079 (2005).

- ⁴⁹K. A. Murphy, N. Reiser, D. Choksy, C. E. Singer, and H. M. Jaeger, "Freestanding loadbearing structures with z-shaped particles," *Gran. Matter* **18**, 26 (2016).
- ⁵⁰J. Sautel, A. Bourges, A. Caussariou, N. Plihon, and N. Taberlet, "The physics of a popsicle stick bomb," *Am. J. Phys.* **85**, 783–790 (2017).
- ⁵¹A. Kabla and L. Mahadevan, "Nonlinear mechanics of soft fibrous networks," *J. R. Soc. Interface* **4**, 99–106 (2006).
- ⁵²E. Cosserat and F. Cosserat, "Théorie des corps déformables," *Nature* **81**, 67 (1909).
- ⁵³D. M. Kaufman, R. Tamstorf, B. Smith, J.-M. Aubry, and E. Grinspun, "Adaptive nonlinearity for collisions in complex rod assemblies," *ACM Trans. Graph.* **33**, 123 (2014).
- ⁵⁴G. Kirchhoff, "Über das gleichgewicht und die bewegung eines unendlich dunnen elastischen stabes," *J. Reine Angew. Math.* **56**, 285–313 (1859).
- ⁵⁵D. Harmon, E. Vouga, B. Smith, R. Tamstorf, and E. Grinspun, "Asynchronous contact mechanics," in *ACM Transactions on Graphics (TOG)* (ACM, 2009), Vol. 28, p. 87.
- ⁵⁶F. Bertails, B. Audoly, M.-P. Cani, B. Querleux, F. Leroy, and J.-L. Lévêque, "Super-helices for predicting the dynamics of natural hair," in *ACM Transactions on Graphics (TOG)* (ACM, 2006), Vol. 25, pp. 1180–1187.
- ⁵⁷R. Goldenthal, D. Harmon, R. Fattal, M. Bercovier, and E. Grinspun, "Efficient simulation of inextensible cloth," *ACM Trans. Graph.* **26**, 49 (2007).
- ⁵⁸J. M. Kaldor, D. L. James, and S. Marschner, "Simulating knitted cloth at the yarn level," in *ACM Transactions on Graphics (TOG)* (ACM, 2008), Vol. 27, p. 65.
- ⁵⁹D. Durville, "Numerical simulation of entangled materials mechanical properties," *J. Mater. Sci.* **40**, 5941–5948 (2005).
- ⁶⁰A. Garg, A. O. Sageman-Furnas, B. Deng, Y. Yue, E. Grinspun, M. Pauly, and M. Wardetzky, "Wire mesh design," *ACM Trans. Graph.* **33**, 66 (2014).
- ⁶¹Y. Yang, I. Tobias, and W. K. Olson, "Finite element analysis of dna supercoiling," *J. Chem. Phys.* **98**, 1673–1686 (1993).
- ⁶²C. W. Wolgemuth, T. R. Powers, and R. E. Goldstein, "Twirling and whirling: Viscous dynamics of rotating elastic filaments," *Phys. Rev. Lett.* **84**, 1623 (2000).
- ⁶³W. Ko, S. Lim, W. Lee, Y. Kim, H. C. Berg, and C. S. Peskin, "Modeling polymorphic transformation of rotating bacterial flagella in a viscous fluid," *Phys. Rev. E* **95**, 063106 (2017).
- ⁶⁴S. J. Gerbode, J. R. Puzey, A. G. McCormick, and L. Mahadevan, "How the cucumber tendril coils and overwinds," *Science* **337**, 1087–1091 (2012).
- ⁶⁵M. Islam, G. Tudryn, R. Bucinell, L. Schadler, and R. Picu, "Stochastic continuum model for mycelium-based bio-foam," *Mater. Des.* **160**, 549–556 (2018).
- ⁶⁶J. Linn, T. Hermansson, F. Andersson, and F. Schneider, "Kinetic aspects of discrete cosserat rods based on the difference geometry of framed curves," in *ECCOMAS Thematic Conference on Multibody Dynamics, Prague, Czech Republic* (2017).
- ⁶⁷C. Armanini, F. Dal Corso, D. Misseroni, and D. Bigoni, "From the elastica compass to the elastica catapult: An essay on the mechanics of soft robot arm," *Proc. R. Soc. A* **473**, 20160870 (2017).
- ⁶⁸M. Gazzola, L. Dudge, A. McCormick, and L. Mahadevan, "Forward and inverse problems in the mechanics of soft filaments," *R. Soc. Open Sci.* **5**, 171628 (2018).
- ⁶⁹G. J. Pagan-Diaz, X. Zhang, L. Grant, Y. Kim, O. Aydin, C. Cvetkovic, E. Ko, E. Solomon, J. Hollis, H. Kong *et al.*, "Simulation and fabrication of stronger, larger, and faster walking biohybrid machines," *Adv. Funct. Mater.* **28**, 1801145 (2018).
- ⁷⁰N. Charles, M. Gazzola, and L. Mahadevan, "Topology, geometry and mechanics of strongly stretched and twisted filaments," [arXiv:1905.00796](https://arxiv.org/abs/1905.00796) (2019).
- ⁷¹O. Aydin, X. Zhang, S. Nuethong, G. J. Pagan-Diaz, R. Bashir, M. Gazzola, and M. T. A. Saif, "Neuromuscular actuation of biohybrid motile bots," *Proc. Natl. Acad. Sci. U.S.A.* **116**, 19841 (2019).
- ⁷²X. Zhang, F. Chan, T. Parthasarathy, and M. Gazzola, "Modeling and simulation of complex dynamic musculoskeletal architectures," *Nat. Commun.* **10**, 4825 (2019).
- ⁷³M. Islam, G. Tudryn, R. Bucinell, L. Schadler, and R. Picu, "Morphology and mechanics of fungal mycelium," *Sci. Rep.* **7**, 13070 (2017).
- ⁷⁴Y. Dothan, see https://commons.wikimedia.org/wiki/File:Lotan1_050.jpg for more information about "Lotan1 050."
- ⁷⁵K. Dierichs and A. Menges, "Granular construction: Designed particles for macro-scale architectural structures," *Archit. Des.* **87**, 88–93 (2017).
- ⁷⁶G. Verhille, S. Moulinet, N. Vandenberghe, M. Adda-Bedia, and P. Le Gal, "Structure and mechanics of aegagropilae fiber network," *Proc. Natl. Acad. Sci. U.S.A.* **114**, 4607–4612 (2017).
- ⁷⁷P. Aejmelaeus-Lindström, A. Mirjan, F. Gramazio, M. Kohler, S. Kernizan, B. Sparrman, J. Laucks, and S. Tibbits, "Granular jamming of load-bearing and reversible structures: Rock print and rock wall," *Archit. Des.* **87**, 82–87 (2017).
- ⁷⁸Close-up of a piece of textile-reinforced concrete.
- ⁷⁹G. Retain, "Something else, something raw: From protohouse to blokhut—The aesthetics of computational assemblage," *Archit. Des.* **86**, 84–89 (2016).
- ⁸⁰E. Steltz, A. Mozeika, N. Rodenberg, E. Brown, and H. M. Jaeger, "Jsel: Jamming skin enabled locomotion," in *2009 IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS)* (IEEE, 2009), pp. 5672–5677.
- ⁸¹A. J. Loeve, O. S. van de Ven, J. G. Vogel, P. Breedveld, and J. Dankelman, "Vacuum packed particles as flexible endoscope guides with controllable rigidity," *Gran. Matter* **12**, 543–554 (2010).
- ⁸²J. D. Brigido-González, S. G. Burrow, and B. K. Woods, "Switchable stiffness morphing aerostructures based on granular jamming," *J. Intell. Mater. Syst. Struct.* **30**, 2581–2594 (2019).
- ⁸³K. Dierichs and A. Menges, "Towards an aggregate architecture: Designed granular systems as programmable matter in architecture," *Gran. Matter* **18**, 25 (2016).
- ⁸⁴P. Aejmelaeus-Lindström, J. Willmann, S. Tibbits, F. Gramazio, and M. Kohler, "Jammed architectural structures: Towards large-scale reversible construction," *Gran. Matter* **18**, 28 (2016).
- ⁸⁵S. Keller and H. M. Jaeger, "Aleatory architectures," *Gran. Matter* **18**, 29 (2016).
- ⁸⁶L. T. Choong, M. M. Mannarino, S. Basu, and G. C. Rutledge, "Compressibility of electrospon fiber mats," *J. Mater. Sci.* **48**, 7827–7836 (2013).
- ⁸⁷D. Roylance, "Ballistics of transversely impacted fibers," *Text. Res. J.* **47**, 679–684 (1977).
- ⁸⁸P. M. Cuniff, M. A. Auerbach, E. Vetter, and D. J. Sikkema, "High performance "M5" fiber for ballistics/structural composites," in *23rd Army Science Conference* (Citeseer, 2002), p. 1e8.
- ⁸⁹See <https://inhabitat.com/cantilevering-protobhouse-is-a-fibrous-3d-printed-home-waterproofed-on-the-inside/> for more information about "Protohouse: A cantilevered, fibrous home created with a 3d printer."
- ⁹⁰See <https://inhabitat.com/drones-weave-moth-inspired-pavilion-from-carbon-fiber-threads/> for more information about "Drones weave moth-inspired pavilion from carbon fiber threads."
- ⁹¹See <https://www.abc.net.au/news/2016-01-11/straw-bale-house-using-pre-fabricated-panels-under-construction/7081432> for more information about "Straw bale house using pre-fabricated panels under construction."
- ⁹²L. E. Biddle, D. C. Deeming, and A. M. Goodman, "Morphology and biomechanics of the nests of the common blackbird *turdus merula*," *Bird Study* **62**, 87–95 (2015).
- ⁹³D. C. Deeming, M. C. Mainwaring, I. R. Hartley, and S. J. Reynolds, "Local temperature and not latitude determines the design of blue tit and great tit nests," *Avian Biol. Res.* **5**, 203–208 (2012).
- ⁹⁴D. C. Deeming, "Importance of nest type on the regulation of humidity in bird nests," *Avian Biol. Res.* **4**, 23–31 (2011).
- ⁹⁵M. Hansell, *Bird Nests and Construction Behaviour* (Cambridge University Press, 2000).
- ⁹⁶N. Collias, "Engineering aspects of nest building by birds," *Endeavour* **10**, 9–16 (1986).
- ⁹⁷C. B. Heenan and R. S. Seymour, "Structural support, not insulation, is the primary driver for avian cup-shaped nest design," *Proc. R. Soc. B* **278**, 2924–2929 (2011).
- ⁹⁸P. T. Walsh, M. Hansell, W. D. Borello, and S. D. Healy, "Are elaborate bird nests built using simple rules?," *Avian Biol. Res.* **6**, 157–162 (2013).
- ⁹⁹F. Muth and S. D. Healy, "Zebra finches select nest material appropriate for a building task," *Anim. Behav.* **90**, 237–244 (2014).
- ¹⁰⁰I. E. Bailey, K. V. Morgan, M. Bertin, S. L. Meddle, and S. D. Healy, "Physical cognition: Birds learn the structural efficacy of nest material," *Proc. R. Soc. B* **281**, 20133225 (2014).